

**Article type:** Review

## **Bioprinting 101: Design, Fabrication and Evaluation of Cell-laden 3D Bioprinted Scaffolds**

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This paper has been peer-reviewed and accepted for publication, but has yet to undergo copyediting and proof correction. The final published version may differ from this proof.

Tissue Engineering

Bioprinting 101: Design, Fabrication and Evaluation of Cell-laden 3D Bioprinted Scaffolds (DOI: 10.1089/ten.TEA.2019.0298)

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Keywords: 3D bioprinting, bioink, hydrogels, additive manufacturing

## Abstract

3D Bioprinting is an additive manufacturing technique that recapitulates the native architecture of tissues. This is accomplished through the precise deposition of cell-containing bioinks. The spatiotemporal control over bioink deposition permits for improved communication between cells and the extracellular matrix (ECM), and facilitates fabrication of anatomically and physiologically relevant structures. The physiochemical properties of bioinks, before and after crosslinking, are crucial for bioprinting complex tissue structures. Specifically, the rheological properties of bioinks determines printability, structural fidelity and cell viability during the printing process, whereas post-crosslinking of bioinks are critical for their mechanical integrity, physiological stability, cell survival, and cell functions. In this review, we critically evaluate bioink design criteria, specifically for extrusion-based bioprinting techniques, to fabricate complex constructs. The effects of various processing parameters on the biophysical and biochemical characteristics of bioinks are also discussed. Furthermore, emerging trends and directions for future development in the area of bioinks and bioprinting are also highlighted.

## Impact

Extrusion-based 3D bioprinting is an emerging additive manufacturing approach for fabricating cell-laden tissue engineered constructs. This review critically evaluates bioink design criteria to fabricate complex tissue constructs. Specifically, pre- and post- printing evaluation approaches are described, as well as new research directions in the field of bioink development and bioprinting are highlighted.

## 1. Introduction

Additive manufacturing is a layer-by-layer fabrication process to construct complex three-dimensional (3D) objects.(1) 3D Bioprinting, an emerging category of additive manufacturing, focuses on precise deposition of cell-laden hydrogel bioinks to construct tissue engineered structures (**Figure 1a**).(2) A multitude of 3D bioprinting techniques have been developed, including laser-assisted printing,(3, 4) inkjet printing(5, 6) and extrusion-based printing(7, 8). Amongst these different approaches, extrusion-based 3D bioprinting has become a popular technique as hydrogel precursors with low-shear viscosities ( $>10^2$  Pa-s) can be used for bioprinting.(9-11) Additionally, 3D bioprinting is also being explored for designing a range of tissue types for regenerative medicine (**Figure 1b**). (12)

One of the primary components of 3D bioprinting is hydrogel bioinks. Hydrogels are water swollen polymeric networks that can be engineered to control various cellular functions such as adhesion, spreading, proliferation and differentiation.(13-19) Hydrogels exhibit cytocompatibility and are extensively used to design cell-laden constructs.(13, 14) Recent developments in hydrogel chemistries, reinforcement approaches, and crosslinking methods have expanded the applications of 3D bioprinting to pharmaceuticals, regenerative medicine and biomedical devices (**Figure 1c**). Thus, it is imperative to understand the fundamental relationships between hydrogel formulation, biophysical characteristics and cellular interactions in 3D microenvironments.(20-22) Furthermore, bioink characterization in terms of swelling, degradation, and flow properties will provide insight about the performance of bioinks and 3D printed structures in physiological conditions.(23, 24)

In this review, we discuss biophysical and biochemical characteristics of bioinks and their relationship to the extrusion-based 3D bioprinting process. Specifically, bioink characteristics at different stages of the bioprinting process are highlighted. We attempt to elucidate mechanical properties, cell-material interplay and the effects of processing parameters on cellular viability in the bioprinting process. Finally, promising new research directions in the field of bioprinting are also summarized.

## 2. Extrusion-based 3D Bioprinting

In extrusion-based 3D bioprinting, a nozzle continuously extrudes the bioink filament, and enables deposition in pre-defined geometries. During the extrusion process, the bioink should possess low viscosity to prevent possible clogging of the extrusion tips (needle) as well as protect cells from excessive fluid shear stress. Upon deposition on the printer bed, the bioink should undergo rapid solidification to maintain the deposited shape.(25, 26) The resolution through extrusion bioprinting is generally between 50 - 1000  $\mu\text{m}$ .(27, 28) The process of extrusion based bioprinting involves considerations at three different stage of bioprinting. The crucial bioink characteristics at pre-extrusion stage include precursor viscosity, cell distribution and biocompatibility.(29) The critical bioink attribute at mid-extrusion stage considers shear stress minimization through plug flow behavior and post-extrusion stage includes physiological stability post crosslinking of 3D printed structures **(Figure 2a)**.(7, 30, 31) Careful control of biomaterial chemistry determines stiffness and dictates the processing capability of the bioink. The potential to deposit high cell densities, matching the physiological structure, is a major advantage of extrusion-based bioprinting.(32, 33) Hence, designing appropriate bioinks is crucial for obtaining 3D prints with relevant resolution, fidelity, cell density and other essential properties.(34)

### 2.1. Bioinks and the Biofabrication Window#

Bioinks for extrusion-based 3D bioprinting need to withstand high shear forces during the extrusion process and recover rapidly thereafter. Typically, polymer formulations that stabilize rapidly, such as gelatin methacryloyl (GelMA)(35, 36) or alginate,(37, 38) have been used. To design bioinks for 3D bioprinting, the concept of the biofabrication window has been traditionally utilized. The biofabrication window describes the trade-offs between printability and cell viability within the constructs **(Figure 2b)**. It details the compromise in bioink design that is made to devise bioinks with suboptimal printability while maintaining cellular activity.(39) Advanced bioinks employ numerous strategies to elevate printability and cellular compatibility simultaneously. Such advanced bioink formulations are designed with shear-thinning abilities, which modulate viscosity during bioprinting process and allow the bioink to regain its original viscosity post extrusion.

Advanced bioinks also protect the encapsulated cells without compromising the printability or print fidelity.(40)

## 2.2. Bioprinting Considerations

A range of biophysical, and biochemical attributes of bioinks can influence 3D printability. These properties include shear-thinning, recoverability, gelation kinetics, biocompatibility, and biodegradation. Prior to printing, computer aided design (CAD) files are used to design the construct to be printed. CAD software provides an array of tools to create complex and anatomically relevant structures. CAD files are subsequently converted to g-code, which communicates the desired printing path and parameters (i.e. speed, location, infill) to the 3D printer.(41) The bioprinting speed is regulated and is usually between  $700 \text{ mm}\cdot\text{s}^{-1}$  -  $10 \mu\text{m}\cdot\text{s}^{-1}$ .(42, 43) Subsequently, bioinks are loaded into extrusion barrels for bioprinting. Mechanical properties, such as viscosity and shear thinning ability of bioinks, are critical to improve cell viability when exposed to the printing stresses make it possible to extrude the material with minimal applied stress.(44) The usual viscosities of bioinks for extrusion based bioprinting are between  $30 - 6 \times 10^7 \text{ mPa}\cdot\text{s}$ .(45, 46) Once loaded, bioprinting commences, depositing cell-laden bioinks onto the printer bed. Crosslinking chemistry determines the ability of the hydrogel to form a stable structure.(31, 47) Biomechanical considerations of the printed constructs include elastic moduli and mechanical integrity.(48, 49) Throughout the printing process, coordinating cell-material interactions, maintaining appropriate rheological characteristics, and maintaining a sterile microenvironment govern the success of the 3D bioprinting process.(50, 51) Extrusion based bioprinting is commonly successful in ensuring long-term high cell viability ( $\sim 80 - 90\%$ ) in the 3D printed constructs.(52-54) Biochemical considerations of the bioprinted structures include degradability, cell-instructive matrix remodeling, and extracellular matrix (ECM) production (**Figure 2c**).(55, 56) Throughout different stages of the bioprinting process, various techniques can be used to measure performance and efficacy. For example, shear-rate sweeps can determine if a material has potential to be injectable, and cytotoxicity assays indicate if a material has favorable interactions with cells.(57-59) The proceeding sections will examine the various approaches used to characterize and quantify the utility bioinks for fabricating intricate, complex geometries.

### 3. Bioink Design and Pre-Printing Considerations

3D Bioprinting of hydrogel bioinks involves more complex design criteria as compared to typical fabrication techniques. For example, bioinks (hydrogel precursors) must be transported through a needle and be able to retain a deposited shape upon extrusion. Appropriate polymer selection is essential to maintain viability of encapsulated cells and achieve the necessary mechanical requirements for 3D printing.(50)

#### 3.1. Polymer Selection

Bioink composition should support high viability of encapsulated cells and shield cells from shear stress during extrusion.(50, 60-64) Molecular weight and crosslinking density remain the two most critical physical characteristics that influence cell behavior, regardless of the polymer used. (63, 64) Naturally derived polymers, such as gelatin and alginate, have well characterized crosslinking-mechanisms and mechanical properties (as a crosslinked hydrogel). (65-68) Naturally derived polymers often exhibit high molecular weights, while synthetic polymers have custom molecular weights.(69, 70) However, natural polymers, such as gelatin or gelatin methacryloyl (GelMA) present integrin-binding motifs, facilitating strong bioink-cell interactions. Gelatin with different 'bloom strength' reflects the average molecular weight of the polymer. Higher bloom strength indicates formation of stiffer gels. Conversely, synthetic polymers, like poly(ethylene glycol) (PEG), permit for finely tuned molecular weights ranging from <500 to >1,000,000 Da, which can be leveraged to control mesh size and nutrient diffusion. Due to the chemical formula (-CH<sub>2</sub>-CH<sub>2</sub>-O-) of the PEG backbone, it is often considered a biologically inert "blank slate" polymer that will interact minimally with cells and the body.(71) However, PEG must be chemically modified in order to crosslink and form stable hydrogels. Both dimethacrylate and diacrylate PEG have been among the most widely studied model hydrogels.(72) Nuclear magnetic resonance (NMR) spectroscopy or attenuated total reflectance (ATR) can be used to verify the terminal end groups of the polymer and molecular weight of the polymer. Overall, bioinks must meet the needs of being able to mechanically deform and re-form while also providing an environment for cell proliferation. Achieving a synergistic balance of all the properties is required to maintain printability with active cellular viability and proliferation.(73)

Polymer selection is also influenced by the type of functionalities desired. Molecular weight influences cell behavior due to the amount of swelling a hydrogel may undergo, resulting in nutrient supplementation and waste removal.(74) Matrix degradability is another factor that plays a significant role in polymer selection.(39, 75) Natural polymers derivatives, like GelMA, contains degradation sites sensitive to matrix metalloproteinases (MMP). MMPs allow natural cleaving of ECM components permitting cells to remodel and degrade the matrix.(76, 77) The end-groups of the polymers determine the crosslinking mechanism that must be employed. Acrylate end groups have historically been common as they provide a facile method (UV curing) for creation of covalent crosslinks. Similarly, thiol end groups are also involved in unique crosslinking such as thiol-ene click chemistry(78) and thio-nanoparticle vacancy driven gelation(79). Some of the common polymer types utilized, their crosslinking approaches and desired functionalities are summarized (**Figure 3a**).

Polymer dispersity index (PDI) is another important factor affecting the overall bioink properties. Polymer molecular weight is critical to control bioink flow characteristics and the resulting mechanical and biocompatibility properties.(80) Having low PDI, suggest that the polymer is similar in length, resulting in consistent mechanical properties.(81) Due to processes variations, natural polymers are typically more polydisperse than synthetic polymers. (82, 83) Increasing polymer molecular weight, crosslink density, or concentration can improve the printability of the solutions at the cost of limited cell migration and a reduction in nutrient diffusion.(84) Polymer molecular weight, crosslinking mechanism, and side-groups dictate functionality of the polymer as a bioink and subsequent compatibility.(85) High molecular weight polymers are typically viscous due to an increase in chain entanglements.(86) Further, many of these characterization techniques can be used to measure the overall bioprinting process and the interplay between material chemistry and mechanical stresses cell undergo during the printing process.

### 3.2. Rheology of Bioinks

As extrusion-based bioinks must be injected through a printing gauge, the ability to flow is of utmost importance. Rheology is the study of flow properties of materials under external



forces.(87) Unfortunately, rheology data presented often lacks the contextual relationship of the rheology to the printing results. Recent studies are beginning to understand the correlation that exists between the rheology of bioinks and the subsequent shape fidelity.(88) Here, we present an understanding of the various rheological tests that are available, their ability to predict potential of a bioink for 3D bioprinting (**Figure 3b**), and the parameters that are often lacking in current studies.

Rheological characteristics of bioinks are determined using either a stress or a strain-controlled rheometer. Rheometers either apply a specific displacement or force, both of which can either be applied in oscillation (back and forth) or in rotation (unidirectional). Various parameters such as storage modulus ( $G'$ ), loss modulus ( $G''$ ), and viscosity ( $\eta$ ) are calculated and can be used to define the printability of bioink formulations.(87, 89) Storage modulus is a measure of the elastic energy within the bioink, while loss modulus is a measure of the viscous portion or dissipated energy within the bioink.(39) Both storage and loss modulus are calculated while performing oscillatory measurements. Viscosity, calculated *via* rotational tests, measures the material's resistance to flow.(90) Typically, bioink characteristics are determined using an oscillatory amplitude or frequency sweep to demonstrate the storage and loss modulus and a rotational shear-rate sweep is performed to determine viscosity.(91) Storage and loss moduli can be determined for pre-crosslinked or post-crosslinked bioinks as a measurement of bioink performance. Viscosity is used to describe the ability of the bioink to flow through the reservoir, needle, and onto the printing surface.(92) After extrusion, a bioink must quickly recover or be crosslinked so that it does not spread on the printing surface.(93) These rheological characteristics are crucial to define the printability of bioink and will be discussed in detail.

### 3.2.1. Viscosity

For extrusion-based bioprinting, a high low-shear viscosity is necessary to ensure the bioink does not spread and prevent collapse of large structures. Viscosity can be controlled by polymer molecular weight, degree of branching, concentration, and addition of rheological modifiers.(94) Generally, an increase in these parameters results in an increase in viscosity across all shear rates. This is illustrated in **Table 1**, which details a list of

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Tissue Engineering  
Bioprinting 101: Design, Fabrication and Evaluation of Cell-laden 3D Bioprinted Scaffolds (DOI: 10.1089/ten.TEA.2019.0298)

commonly used polymers for bioinks. Conversely, lower crosslinking density within hydrogel matrix aids in cell proliferation, migration, and tissue formation through the facilitation of nutrient diffusion and waste removal.(95) Importantly, the viscosity of a hydrogel bioink can directly influence the resulting shape fidelity such as drooping and spreading.

Viscosity influences the ability of bioink to flow. An increase in surface tension between the needle gauge and bioink will decrease the ability of the bioink to shear thin, whereas an ideal, frictionless system will facilitate extrusion.(96) Overall, the bioink viscosity dictates whether extruded materials are droplets, a continuous filament or strand.(36) Low viscosity solutions of GelMA, tend to form droplets that either will be forcefully expelled or form large droplets that gravity causes to separate from the nozzle.(97) However, rheological modifiers, such as nanosilicates(98-100) or hyaluronic acid(97), can be added to GelMA to increase the viscosity and form a filament rather than a droplet. Filament formation allows for high-fidelity 3D structures to be formed rather than a puddle.

### 3.2.2. Shear-Thinning Ability

Shear-rate sweeps are most commonly used to predict the behavior of a bioink during the printing process, determining viscosities across a range of shear rates. A constant shear-rate is applied for each measurement within a shear-rate sweep, thus precisely determining the ability of the bioink to deform. Shear-rate sweeps often apply a range of shear rates, from low shear rate ( $<10^{-3} \text{ s}^{-1}$ ) to high shear rates ( $>10^2 \text{ s}^{-1}$ ), in order to mimic the bioink going through a needle. For bioinks, a high viscosity at low shear rates and low viscosity at high shear rates is imperative for the extrusion process.(101) Materials that exhibit this characteristic are called “shear-thinning”.(8, 102) Often characteristic shear rate versus viscosity graphs are presented with a lack of details. Several models have been developed that can describe the ability of a hydrogel to shear thin. Classically, the power-law model, which is explained through the equation  $\eta = K\dot{\gamma}^{n-1}$ , where  $\eta$  is viscosity,  $K$  is the flow consistency index and  $n$  is the shear-thinning index has been applied to materials where a low shear-rate or high shear-rate viscosity plateau is not observed. The power law index can describe the degree of shear-thinning. When  $n=1$ , the solution is Newtonian;  $n<1$

shear-thinning;  $n > 1$  shear thickening.(103) While graphical interpretation informs readers that materials are shear-thinning, equation fitting may bring broader understanding to the data collected and an overall conclusion regarding the ability of a bioink to be extruded through needles (**Figure 3c**). For example, the rheological profile of alginate precursors have been investigated using the Generalized Power-law equation.(50) Through the application and study of the flow consistency index, it was concluded that  $n \sim 0.3-0.4$  has an appropriate flow profile for bioprinting applications. In addition, the yield stress was examined as a critical parameter that dictates cell viability during the printing process. Other work suggests that hydrogel precursor modulus is important for cell delivery.(104) Uncrosslinked bioink viscosity and storage modulus are analogous measurements, with the viscosity measuring resistance to flow, while storage modulus is an interpretation of hydrogel stability.

The use of shear-thinning information to predict the ability of a bioink to be 3D printed has also been investigated. We would like to make the important distinction of being able to inject materials versus 3D printed bioinks: 3D printing requires a bioink to stabilize or localize at a given point, while injection only requires materials to be shear-thinning. Once the bioink has exited the needle, there are little to no shear-forces exerted on the bioink.(105) To achieve more accurate rheological predictions for 3D bioprinting applications, researchers are encouraged to calculate the shear-rates experienced throughout the 3D printing process, program rheological tests to apply these specific shear-rates, and examine the viscosity recovery. In a recent study, a recovery time of 30s was deemed appropriate and percentage recovery was measured as a comparison between un-sheared and post-sheared bioinks.(106) Researchers often use hydrogel precursors during the extrusion process, utilizing viscosity as the defacto measurement of choice via a rheometric viewpoint. Additionally, thixotropic loops (increasing shear rate followed by a decreasing shear rate in a set amount of time) describe the internal structure rebuilding time.(107, 108) A perfectly Newtonian bioink will have overlapping curves for both the increasing and decreasing shear rates, indicating the presence of a minimal internal structure and a non-ideal bioink candidate.(108) A difference between loading and unloading curves indicates the degree of thixotropic behavior within the

context of the test (i.e. if the test was completed using a one-minute loading and one-minute unloading curve, thixotropy is specific to the time frame applied).(109) Thixotropic loop tests can be difficult to interpret and often require specialized “cup and cone” geometries to obtain reliable results.

### 3.2.3. Yield Stress

Bioinks must overcome a certain amount of stress, deemed yield stress, to allow for flow from the barrel and onto the printing bed. Yield stress is the minimum stress that must be placed on the material for flow to occur. Hydrogel precursors are typically a weak network. When a stress is applied above the yield stress, these network interactions are interrupted, permitting the material to flow.(110, 111) For example, gelatin is a thermo-responsive hydrogel, and above  $\sim 37^{\circ}\text{C}$  it has high chain motility due to weak polymer-polymer interactions and can easily be extruded through a needle when stress is applied. High yield stresses pose process difficulties in cell incorporation and in the work required for the 3D printer motor. Along with gelatin, other hydrogels, such as a self-assembling peptide (112, 113) and colloidal systems,(114, 115) have been developed that incorporate lower yield stress as an important design consideration.

Oscillatory thixotropic measurements further elucidate bioink stability during printing process. To complete oscillatory thixotropy measurement, an amplitude sweep must first be conducted to determine the linear viscoelastic regime of a bioink. Specifically, the storage modulus and loss modulus should be independent of the applied stress or strain (both of which are amplitude modulated). Outside of the linear regime, the bioink is dependent on higher order harmonics, requiring more advanced knowledge for data interpretation. A yield point, where the storage modulus decreases below the loss modulus ( $G' < G''$ ) is exhibited, is typically demonstrated at amplitudes above  $10^1$  Pa or between 50-1000% strain.(116) Oscillatory thixotropic tests, also known as peak-hold tests, apply series of sequential amplitudes, simulating printing conditions. First, an amplitude below the yield point is applied, representing  $G' > G''$ . This is followed by application of a higher amplitude ( $G'' > G'$ ), which represents the flow through the needle. The last step is application of the original amplitude, with the expectation that  $G'$  will

increase quickly back to the original value.(117) Traditionally, researchers have tested multiple cycles, although the 3D printing process requires only one application of a high amplitude since the bioink must only traverse the length of the needle once.

### 3.3. Print Fidelity

Bioink composition is extremely crucial in designing prints with high resolution and fidelity. High viscosities at low-shear rates dictate construct fidelity. Often, bioinks lack recoverability, resulting in printed structures with lower resolutions and accuracies than can be achieved with other additive manufacturing techniques. However, when shear-thinning behavior, yield stress, and recoverability are examined holistically, high fidelity prints can be achieved. Achieving a synergistic balance between shear-thinning, yield stress, and shear recoverability is required as the complexity of printing increases from 1D to 3D (**Figure 3d**).(118) Another important parameter which governs fidelity of constructs is the swelling behavior of the hydrogel ink, which is mainly determined by the charge densities and extent of crosslinking.(97, 119) High crosslinking densities support lower swelling ratios and provide high fidelity prints but reduce oxygen and nutrients diffusion, thereby reducing cell viability in the constructs. A solution to this problem is to design a composite bioink combining hydrogel materials which provide enhanced cell activity with a material that confers mechanical stability, thus arriving at good print fidelity.(120)

## 4. Post Printing Considerations and Assessment

Upon establishing cytocompatibility, the bioink can be printed into complex shapes and geometries. However, there are additional biological and mechanical characteristics that need to be taken into consideration post-printing.

### 4.1. Physiological Stability of 3D Bioprinted Structures

#### 4.1.1. Structural Fidelity

Rheology is an important tool to determine the potential of a bioink for printing, specifically characterizing the ability of the bioink to deform and recover. However, after printing, image analysis of extruded bioinks provides additional information concerning spreading of bioinks (**Figure 4a**). Several methods have been employed to analyze the quality of extrudate. The 3D printing process begins in designing a construct in a computer

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aided design program (i.e. AutoCAD or Solidworks).(121) Given the programmed design and dimensions, the print fidelity can be characterized by comparing the experimental, extruded dimensions to the theoretical ones. Light microscopy or micro-computed tomography ( $\mu$ CT) has been used to image printed constructs.(117, 122) Ouyang et al. devised a system of images and equations to quantify the “printability” of extruded bioinks.(123) Three classes of printability were established (under gelation, proper gelation, and over gelation) to describe the morphology of the extruded samples. Proper gelation bioinks exhibited smooth surfaces with regular grid patterns; under gelation bioinks flowed together creating circle patterns rather than squares; over gelation bioinks had irregular grid patterns. Mathematically, printability ( $Pr$ ) was defined as  $Pr = \frac{\pi}{4} \frac{1}{C} = \frac{L^2}{16A}$ , where  $C$  is the circularity of the print,  $L$  is the length, and  $A$  is the area.  $Pr$  values  $< 1$  indicate poor fidelity with spreading and large, curved corners. As  $Pr$  approaches 1, the print “exactly matches and corresponds to the model design,” with precise angles, smooth prints, and exact deposition of material. As  $Pr$  increases, the bioink became jammed or “crinkly”/rough (ridges formed, cracks were prominent, and the overall print was poorly constructed). Mathematically defining print fidelity is an important milestone within the bioprinting literature. However, printability is defined in only 1D or 2D, and there is a need to develop new approaches to evaluate 3D printability.

#### 4.1.2 Mechanical Stability and Elasticity

Native tissue moduli are well characterized. Therefore, composing a material to match should, in essence, provide mechanical stability of the implanted hydrogel.(124-126) Elastic moduli characterization is a classic method to study the ability of bioink to withstand deformation. Elastic moduli can be determined from the slope of a stress versus strain curve in compression or tension (**Figure 4b**). However, there are discrepancies or limitations between the parameters defined within each test (i.e. compression/tension). For example, when defining the ultimate tensile/compression stress, the range of strain over which testing is performed is limited. Specifically, a material can only be compressed ~90-99%, while under tension the construct can be theoretically stretched indefinitely. The bioprinting process deposits bioink layers that must adhere to each other to form a mechanically rigid structure. The potential for delamination of layers due to low adhesion

results in a defect, thus increasing the chance for stress concentrators and crack propagation.(127, 128) Mechanical compression/tension testing can be performed to evaluate the mechanical properties of 3D printed structures compared to bulk properties. Compression testing of cast bioinks ensures that the structure does not have void spaces within the tested samples (assuming no bubbles, sufficient layer contact, and clean removal from the printing bed). Casted bioinks typically have low polymer alignment since the material is allowed to conform to the surrounding mold. However, due to the layer-by-layer material deposition in the 3D printing process, void spaces can develop or the polymer may align, ultimately producing a significantly different mechanical profile. Ideally, the printed sample should possess 100%-layer adhesion and contact. However, when using a circular gauged needle there might be some space due to a geometric mismatch. From these spaces, cracks propagate and decrease the compressive modulus.(129)

#### 4.1.3. Swelling and Degradation

Once the bioink is crosslinked and placed into either an implanted site or in cell-culture media, swelling of the structure occurs. Swelling can influence post-printing mechanics: an increase in fluid increases the distance between crosslink or net points and decreases crosslink density.(130) Swelling can also be beneficial, as it allows for diffusion of any entrapped therapeutics and cellular waste products.(131) Bioinks composed of natural polymers such as gelatin will both swell and degrade due to enzymes secreted by cells. Gelatin-based hydrogels have previously been used for bioinks, demonstrating a mass loss of 65% within 11 hours when submerged in a collagenase solution (5 U/mL).(132) Synthetic bioinks must be designed to degrade within an appropriate time-scale for the intended application. Poly (lactide-co-glycolide) compositions are often used to regulate the degradation profile of hydrogels or nanoparticles (133, 134) and for drug delivery applications.(135, 136) Specifically, therapeutic release profiles can be modulated via encapsulation into PLGA nanoparticles with varying amounts of lactide and glycolide to allow for appropriate release times.(136) Alternatively, PEG has been modified with poly (lactic acid) end groups (PLA) to modulate network degradation(137, 138) and cell adhesion(139) and proliferation.(140) In order to fully recapitulate native tissue,

degradation profiles are a key feature of developed bioinks that must be characterized further. Hence, swelling and degradation characterization of bioprinted constructs become crucial for understanding their behavior *in vivo* (**Figure 4c**).

#### 4.2. Effect of the Printing Process on Cell Viability

Estimation of cellular compatibility is an essential part to understand bioink-cell interactions and how the cells can be stimulated by the bioink. It is also important to evaluate the effect of shear-forces and degradation byproducts on the bioprinted system. This is done through various cellular cytotoxicity/viability assays (**Figure 5a**). The use of nanoparticles as rheological modifiers to bioink systems also creates challenges in terms of cellular toxicity. Unlike polymeric components of bioinks, whose behavior when interacting with cells is well documented, nanoparticles can interact with cells in many different ways, such as interaction with cytosolic proteins, effects on mitochondrial activity, and generation of reactive oxygen species (ROS). Hence, it is paramount to identify concentration-dependent effects the nanoparticles have on the cells before use in printing applications.(141) These factors are also important for understanding the effects of polymer crosslinking agents on overall cellular viability.(142) A list of common assays used to determine cellular viability within printed constructs is in **Table 2**. However, a major drawback of these assays is the focus only on the cell viability and the lack of consideration of other processes such as cell differentiation, formation of cell signaling molecules, or secretion of proteins.(143) Advanced genetic testing, such as RNA-sequencing, may also be used to identify the effect of bioink components on cells, but this process is both expensive and time consuming.(144)

During 3D bioprinting, encapsulated cells experience shear forces during the bioprinting process which can affect cellular viability, adhesion, and proliferation.(50, 104) Cell suspensions in high viscosity bioinks have been used to increase cell viability.(104) Along with viscosity, geometric constraints of the printing apparatus, such as the needle gauge shape and size, can influence the shear stress being applied to the material: large-orifice deposition needles (small gauge number) reduce the shear stress, while simultaneously reducing resolution of the 3D print, and lower volumetric flow rates decrease the shear stress.(145) Shear stress has profound effects on cell phenotype and functionality. For



example, at 1 Pa of shear stress, articular chondrocytes can significantly change morphology and metabolic activity,(146) whereas human mesenchymal stem cells (hMSCs) can withstand shear stresses in the range of  $1 \times 10^{-5}$  –  $1 \times 10^{-4}$  Pa before significantly upregulating mRNA expressions of osteocalcin, Runx2, and alkaline phosphatase (147). In conjunction with the flow behavior of the bioink, internal shear stress can influence cell viability. Mechano-transduction at the cell-material interface and the mechanical stress placed on cells within the bioink continue to be hurdles for 3D bioprinting constructs. Current techniques to study cell viability as a function of shear stress rely on 2D culture and varying the flow rate of media above the cells. Short term, high shear stress, with cells suspended in a moving medium is less studied, although cells appear to be resilient to the printing process.(148, 149) Bioinks such as GelMA (97, 150), alginate (50, 151), and PEG (152, 153) along with materials such as, peptides (154-156), PCL (157-159), kappa-carrageenan (57, 160), and others (161-163) have been extensively explored to comprehend the interplay between printing parameters and cellular response to the bioprinting process. GelMA-based scaffolds were used to 3D print complex shapes (150) and were used to deposit HepG2 cells with favorable viability.(148) Alginate is often used due to its non-immunogenicity, ability to shear-thin, and quick ionic-crosslinking in  $\text{CaCl}_2$  solutions.(164) The effects of bioink compositions (0.5-1.5 wt./vol. %) and printing pressures (0.5-1.5 bar) on cell viability have been investigated.(50) Human mesenchymal stem cells (hMSC) were >60% viable at shear stress >10 kPa, nearing 100% viability with shear stress <5 kPa. In a similar recent work, PEG based bioinks were developed with human dermal fibroblasts. It was found that before a critical flow rate of ~140 mg/s bioinks with a lower mass flow rate exhibited a linear relationship with cell viability and with decrease in mass flow rate, cell viability decreased. This indicated that increase in hydrogel robustness led to a proportional damage on encapsulated cells.(165) Thus, it is crucial to determine the shear rate distribution within the bioink formulations.

### 4.3. Evaluating Cell-Material Interactions

Concurrent with the cellular viability, cell functions such as adhesion, proliferation, and/or differentiation should also be monitored. Cells encapsulated within the bioink can proliferate and deposit nascent extracellular matrix (ECM) that is composed of a complex

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network of proteins (collagen, elastin, laminin and fibronectin), glycoproteins and proteoglycans.(166) This newly deposited ECM can provide structural and biochemical support to encapsulated cells.

The mechanical stiffness and elasticity of the ECM varies from one tissue type to the next, primarily due to changes in the ECM compositions (in particular elastin and collagen), and the stiffness can differ by several orders of magnitudes. For example, the elastic modulus of soft brain tissue is in the range of tenths of a kilopascal (kPa), while calcified bone is in the range of megapascals (MPa)(167). The change in ECM composition in diseased tissue, particular in case of cancer metastasis, is well-documented(168-171). The ECM protein collagen also plays an important role in cellular adhesion. The process of cell adhesion onto the ECM is a complex biochemical process that has be lined to other cellular events such as cell differentiation, cell migration, and the cell cycle.(172) Both ECM cell adhesion sites and mechanical properties are of paramount importance when selecting biomaterial constituents. The main goal of a fabricated ECM is to provide adequate sites to the cell for binding, as well as a 3D architecture and mechanical stiffness similar to the native tissue. Careful bioink selection allows for the generation of a 3D architecture that faithfully mimics the native tissue, while allowing for the variation in the overall mechanical stiffness and the chemical properties by changing the bioink composition or concentration.(173)

Most commonly, cell-material interactions are commonly measured via two-dimensional seeding of cells on the bioink surface. While useful, these techniques fail to fully capture the complex interactions when cells are encapsulated with 3D matrices. The 3D encapsulation of cells within hydrogels represents an increasingly complex technique for cell culture, but permits for the fabrication of constructs that further recapitulate the innate cellular architecture of tissue scaffolds for engineering applications.(129) This 3D microenvironment better mimics what cells experience *in vivo*, compared to standard tissue culture. In designing new bioinks for extrusion bioprinting, initial cell screenings continue to be an established method to determine cell-material interactions. Thus, it is important to evaluate cell-matrix interactions as well as deposition of nascent ECM protein using various available techniques.

#### 4.3.1. Cell-Matrix Interactions within 3D Printed Structures

Traction force microscopy (TFM) is used to determine the traction force between cells and materials. Using the traditional TFM techniques, cells are cultured on a clear polyacrylamide gels that are functionalized with adhesive ligands and contain fluorescent beads that are embedded just below the gel surface.(174) When attachment occurs, cells generate a traction force that moves the fluorescent beads. This movement is then quantified by measuring the displacement of the fluorescent bead (**Figure 5b**). This technique has been used to compare cellular forces generated by metastatic breast, prostate, and lung cancer cell lines and their non-metastatic cell line analogs. The traction forces of the metastatic cell lines was found to be higher.(175) After seeding cells, TFM could be used to determine where cells are adhering on the bioinks surface and subsequently moving. However, this requires an optically transparent bioink as well as a flat surface to image. Alternatively, vinculin staining can be used to monitor focal adhesion points and elucidate cell binding.(176)

3D-TFM is a modification to TFM and does not require that cells be on the exterior of the sample being analyzed. 3D TFM can be used to understand cell behavior in 3D cultures (**Figure 5b**). In 3D TFM, fluorescent beads are co-encapsulated with the cells within the bioink. A limitation of this technique is the modification of the bioink's rheological properties due to the addition of fluorescent beads. However, this method can provide valuable insight on cell behavior within a bioink. Fraley et al(177) used this techniques to track the movement of focal adhesion proteins in the 3D matrix and establish their role in cell motility. Transparent samples are preferred due to the ability to clearly visualize the fluorescent beads.

Atomic force microscopy (AFM) probe techniques involve the quantification of how strongly a cell is adhered to the surface of the bioink. The AFM cantilever reaches the cells from micrometers above slowly. The cantilever then makes contact and indents it such that the deflection reaches a set point. The cantilever deflections during this process are recorded as force-distance curves, where the highest force is the cells adhesion strength (**Figure 5c**). This technique can be used to measure both cell-cell adhesion forces and cell-matrix adhesion forces.(178) While using AFM with bioink systems, the cells in the printed

constructs must come in contact with AFM tip. Fully encapsulated cells cannot be sensed utilizing AFM techniques without destruction of the printed construct.(179)

Multiple particle tracking microrheology (MPT) is another technique used to quantify cell-matrix interaction. In this technique, probe particles are embedded in the hydrogel matrix. The brownian motion of the embedded particles is measured and related to rheological properties such as creep compliance and viscosity.(180, 181) PEG based peptide cross-linked hydrogel scaffolds were seeded with human mesenchymal stem cells (hMSCs). MPT data was gathered over a period of time, which aided characterization of spatial remodeling of the hydrogels as the hMSCs migrated.(182) MPT is a crucial technique, which identifies regions in the hydrogel network where cells adhere during matrix degradation and MMP secretion. It also characterizes distances over which cellular matrix remodeling occurs.

#### *4.3.2. Evaluating nascent ECM Production within Printed structure*

Along with the visualizing cell interactions with bioinks, evaluation of deposited matrix and protein quantification enhances the understanding of how cells are behaving. The production and deposition of ECM by cells is an important cellular event. In the case of bioprinting, it becomes essential for cells to produce ECM to facilitate further proliferation within the scaffold. Native ECM is composed of various components, such as proteins (collagen, elastin, and fibronectin) and Glycosaminoglycans (GAGs) (heparan sulphate, chondroitin sulphate etc).(183) Hence, it is important to quantify the production of ECM components in 3D printed scaffolds (**Figure 5d**), as they could mimic the 3D architecture of the native tissues. Various methods can be employed for determining the individual components as listed below.

Collagen is the most abundant protein within the human body and is an important ECM component. The most common methods to estimate collagen production is the quantification of hydroxyproline within a sample. This is done by dissolving the sample in hydrochloric acid, followed by neutralization, and further reaction with reagents such as chloramine T.(184) This method has a distinct drawback of being rather tedious and can greatly be affected by the type of sample. Hence, simpler colorimetric methods have been

developed using dyes such as Sirius Red F3BA, which bind the specifically to collagen and show no specific binding with elastins.(185)

There are five types of GAGs: heparan sulfate (HS), chondroitin sulfate (CS), dermatan sulfate (DS), keratan sulfate (KS), and hyaluronan (HA), of which HS is the most studied.(183) There are two commonly used techniques for the quantification of GAGs, namely Alcian Blue and Dimethylmethylene Blue (DMMB) assay. The latter works on the principle of acid digestion of the polysaccharide followed by reaction with a carbazole, which gives rise to a colored byproduct.(186) However this method has a tendency to overestimate the concentration of the GAGs due to interference from pH buffer components, such as chloride ions (present in PBS).(187) The DMMB assay relies on the ability of sulfated GAGs to bind the cationic dye 1,9-dimethylmethylene blue(188) and, hence, is better suited for GAG quantification. With both collagen and GAG quantification, standardization to the number of incorporated cells provides information regarding how active the cells are and if they are proliferating. Nascent protein deposition within the 3D printed construct can be visualized by adapting a recently developed labelling technique. In this technique, methionine molecules containing azide groups are incorporated into proteins during their synthesis. These labelled proteins are then visualized for a spatiotemporal characterization of nascent protein deposition across the hydrogel matrix environment. (189, 190)

## 5. Future Directions

The field of 3D bioprinting has undergone rapid progress over the last several years. There has been headway in optimizing bioinks which not only provide cell viability and printability but also provide additional tunable functionalities, such as stimuli responsiveness and programmable properties. There has also been progress in expanding the hardware of 3D bioprinting to incorporate synergistic, multi-material printing. In the following sections we will examine the various emerging bioprinting techniques and their attributes which make them attractive in this field.

### 5.1. Multimaterial 3D Bioprinting for Fabricating Complex Architectures

Current printing modalities successfully print relatively complex geometries but are not completely successful at recapitulating the intricate compositions of native tissue structures. Progress in various additive manufacturing techniques has led to the development of multi-material bioprinting.(191-196) Multi-material extrusion printing enables for the deposition of multiple bioinks in a coded, continuous manner to fabricate tissue constructs with a smooth and fast transition between different materials (**Figure 6a**). This enables for printing structures that closely mimic native tissue designs and composition.(197) The multi-extrusion process is calibrated with the motorized stage movement, allowing for deposition of 3D architectures with multiple bioinks in a spatially defined manner. However, resolution and print fidelity still remain significant challenges, which are being met by designing additive manufacturing systems that can precisely control the printing of complex architectures.(50) Theoretical modeling is also being applied to the bioink design. Instructing the experimental design of a tissue structure through modelling is expected to enhance the function and properties of biofabricated tissue structures.(198)

### 5.2. 3D Bioprinting Tissue Models for Pre-clinical Evaluation

Engineered tissue models are becoming an increasingly appealing platform to study various diseases and predict the efficacy of novel therapeutic interventions, potentially reducing or eliminating animal subjects.(199) However, traditional fabrication techniques tend to produce oversimplified constructs and cell microenvironments.(200) The advent of 3D bioprinting allows for engineering of complex, biomimetic in vitro tissue models that can aid in treatment optimization.(201) For example, the tumor microenvironment is considered extremely vital in understanding and regulating tumor metastasis and progression.(202) 3D bioprinted tumor models enable a more precise simulation of the tumor environment and are ideal for pre-clinical studies (**Figure 6b**). A 3D printed co-culture ovarian cancer model was 3D printed in a controlled manner using normal fibroblasts and human ovarian cancer cells (OVCAR-5). It was observed that the 3D printed cancer model established 3D acini with growth kinetics and structures similar to in vivo

development.(203) Despite progress in designing cancer models through 3D bioprinting, there still is a limited scope of engineering models with multi-cellular microenvironments consisting of cancer cells, immune cells, non-cancer cells and vascular cells.

### 5.3. Printing Therapeutics in 3D to Control and Direct Cellular Functions

Progress has also been made in designing bioinks loaded with therapeutics which can be utilized to program cell function within printed constructs. For example, a bioink designed from a hydrolytically degradable polymer poly(ethylene glycol)-dithiothreitol (PEGDTT) and 2D nanosilicates loaded with protein therapeutics demonstrated a shear-thinning rheological profile with enhanced printing fidelity.(204, 205) The anisotropic charge of the 2D nanosilicates enables sequestering of protein therapeutics and facilitates their sustained release within the 3D printed structure (**Figure 6c**). This approach exhibits the potential to engineer intricate 3D tissue structures within regenerative medicine.

### 5.4. 4D Bioprinting for Designing Dynamic Tissues

The process of four-dimensional (4D) bioprinting involves 3D bioprinting structures that change upon exposure to an external stimulus, such as light, heat, or moisture. These triggers allow the constructs to change shape, functionality, or properties with the potential to translate into dynamic motion.(206) With detailed insight on material properties and their stimuli responsive behavior, 4D bioprinting allows for the design of programmable structures with tunable functionalities. Examples of materials used for 4D bioprinting include shape memory polymers (SMPs)(207, 208) and hydrogels.(209, 210) 4D printing with SMP-based inks involves embedding SMP fibers within a matrix to constitute a 3D bi-layer structure. A dynamic shape transformation of these structures can be achieved by heating the construct above the characteristic transition temperature exhibited by the SMP.(211) Heat-activated SMPs have been employed in making 4D printed smart stents, which are deformed to transitory shape, introduced into the body and then transformed back to the original shape with a localized temperature change.(207) In the case of hydrogel-based bioinks, 4D bioprinted composites with a bi-layer framework exhibit controlled deformations that depend on the hydrogel's swelling ratios, elastic moduli, and thickness of the framework.(206) Employing modelling

techniques allows for precise prediction of geometric changes of the configurations and generated movements, enabling design of constructs capable of twisting, folding, and/or curling. These hydrogel bioinks can potentially be utilized to bioprint various functional tissue components, such as printed functioning cardiac tissue (212) or personalized replacement heart valves (**Figure 6d**).

Recently, semisynthetic approaches have been developed to enable photomediated 4D site specific protein patterning. In these techniques, diverse library of homogeneous functionalized proteins were developed with reactive handles for biomaterial modification.(213, 214) Masked based photolithography techniques were utilized to control the protein patterning throughout hydrogel thickness. The photoreversible immobilization of proteins can be extended to growth factors and enzymes enabling a dynamic spatiotemporal regulation of cellular proliferation and protein kinase signaling. These techniques can be utilized to design advanced photoresponsive bioinks for 4D bioprinting.

## 6. Conclusion

3D Bioprinting is a multi-faceted fabrication technique for printing complex tissue or even organ structures. The field of bioprinting is rapidly evolving with applications in engineering, science and regenerative medicine. There has been significant progress in designing intricate biomimetic constructs with cellular functionalities. In general, bioprinting has emerged as a strong high-throughput platform technology to conceive macro and micro-scale bioengineered systems. Although current techniques to assess polymeric bioink functionalities for 3D bioprinting applications are widespread, there is little standardization within the field. Additionally, there remains an overall lack of bioink formulations and methodology for predicting usefulness as a bioink. Clinical application of extrusion-based bioprinting requires bioinks that can be organized to replicate tissue organization, support cell proliferation and differentiation, and degrade at physiological time scales. The rheological properties of bioinks correlate to the systems biological performance, dictating the need for novel and precise analysis techniques to monitor cell/material interactions during the printing process. Optimization of the rheological



properties, specifically yield stress, may permit homogeneous cell incorporation and further boost the printing process. Often high resolution is sought in 3D bioprinting, though recent studies suggest high precision may not be necessary(215, 216). Thus, development of advanced bioink materials and formulations with suitability for multiple cell and tissue types is currently an area of focus.

Overall, there is a need to promote fundamental rheological understanding with utilization of biological techniques specifically to further deepen our insight into extrusion-based 3D bioprinting. Thus, there is a need to develop modern computational techniques that consider the bioink properties and mechanics during fabrication, such as nozzle diameter or printing speed, to provide a more holistic approach to 3D bioprinting. Concurrently, there is a strong sense in the bioprinting community to make the printing modalities more accessible. Hence, there needs to be continued efforts in bringing down the cost of bioprinters and making them more available to a broader scientific group. In the near future, we anticipate development of hybrid bioprinting systems capable of dispensing multiple biomaterials, multiple cell populations, as well as multiple biochemical cues (such as drugs, nutrients and growth factors) bringing us one step closer to whole tissue/organ regeneration. These would also lead to advancement of biomanufacturing technologies with in vivo integration, leading to engineering constructs with enhanced in-vivo efficacy. Furthermore, stimuli responsive bioprinting strategies are also set to transform healthcare and medicine by development of dynamic constructs poised to be utilized in biosensing, bioactuation and biorobotics. Thus, this review attempts to elucidate the 3D bioprinting process, detailing its various attributes. It also attempts to provide a deeper understanding of the mechanics governing bioinks and their subsequent macroscopic properties, such as ability to modulate adhesion, degradation, and therapeutic delivery for executing prints with higher resolution, fidelity, and biocompatibility.

### **Acknowledgments**

AKG would like to acknowledge financial support from the National Institute of Biomedical Imaging and Bioengineering (NIBIB) of the National Institutes of Health (NIH) Director's New Innovator Award (DP2 EB026265) and the National Science Foundation (NSF) Award

(CBET 1705852). The content is solely the responsibility of the authors and does not necessarily represent the official views of the funding agency. The authors would also like to thank Karli Gold and Dr. Uyen Nguyen for their help in editing the manuscript. Some of the images in the manuscript were created with Biorender.com

### **Disclosure Statement**

No competing financial interests exist.

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This paper has been peer-reviewed and accepted for publication, but has yet to undergo copyediting and proof correction. The final published version may differ from this proof.

Tissue Engineering  
Bioprinting 101: Design, Fabrication and Evaluation of Cell-laden 3D Bioprinted Scaffolds (DOI: 10.1089/ten.TEA.2019.0298)

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**Table 1.** Common polymers, viscosities, and crosslinking mechanism for Bioinks

Polymer	Concentration	Crosslinking mechanism	Viscosity Range (Pa·s)	Reference
Methacrylated hyaluronic acid/methacrylated gelatin	6-12%	UV	0.1-10000	(217)
PEG-DA + Laponite	10% PEG-DA, 4% Laponite	UV	1200	(117)
Sodium alginate	3-5%	Ionic	0.6-6.4	(218)
GelMA	3-5%	UV	75-2000	(219)
Hyaluronic Acid	1.5%	Temperature	22	(220)
Collagen	1.5-1.75%	Temperature, pH	1.7-1.8	(221)

**Table 2.** List of common assays to measure cell viability

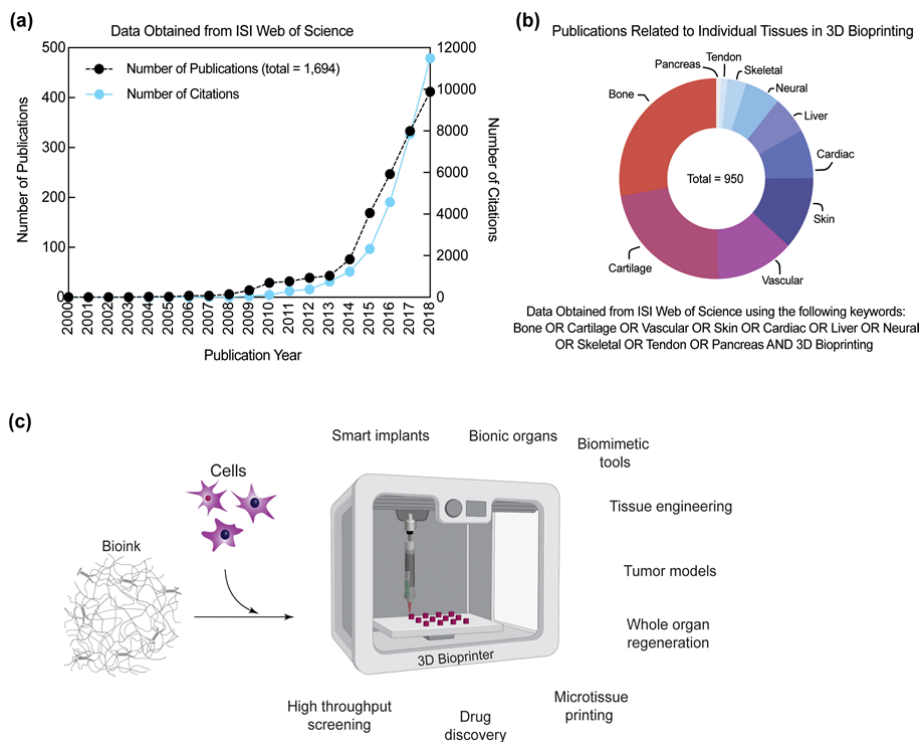
Reagent	Site of action	Method of Detection	Ref
Trypan blue	Cytoplasm	Trypan blue is excluded by live cells with intact plasma membranes, while dead cells are stained blue	(222)
LDH	Extracellular space	Release of LDH (lactate dehydrogenase) cytosolic enzyme into extracellular space. The released LDH is then measured via a tetrazolium dye.	(223-225)
TBARS	Cytoplasm	Estimation of lipid peroxidation due to ROS generation by quantification of Malondialdehyde present in cells.	(226, 227)
Calcein-AM and Ethidium Bromide (Live/Dead assay)	Cytoplasm	Fluorescent probes commonly used together in the form of Live/Dead viability assay. Live cells are able to exclude Ethidium bromide, while dead cells do not show fluorescence for calcein.	(228, 229)
Annexin V	Cell Membrane	Early apoptosis detection, due to movement into the outer membrane of the plasma membrane	(230)
H <sub>2</sub> DFCA	Cytoplasm	The cell-permeant 2',7'-dichlorodihydrofluorescein diacetate (H <sub>2</sub> DCFDA) is reduced to its fluorescent form inside cells in the presence of reactive oxygen species (ROS).	(231, 232)
Comet assay	Nucleus	DNA fragmentation is viewed by single cell gel electrophoresis.	(233, 234)
Micronucleus assay	Nucleus	Study of DNA damage at the chromosome level. By differential staining of DNA and RNA through	(235, 236)

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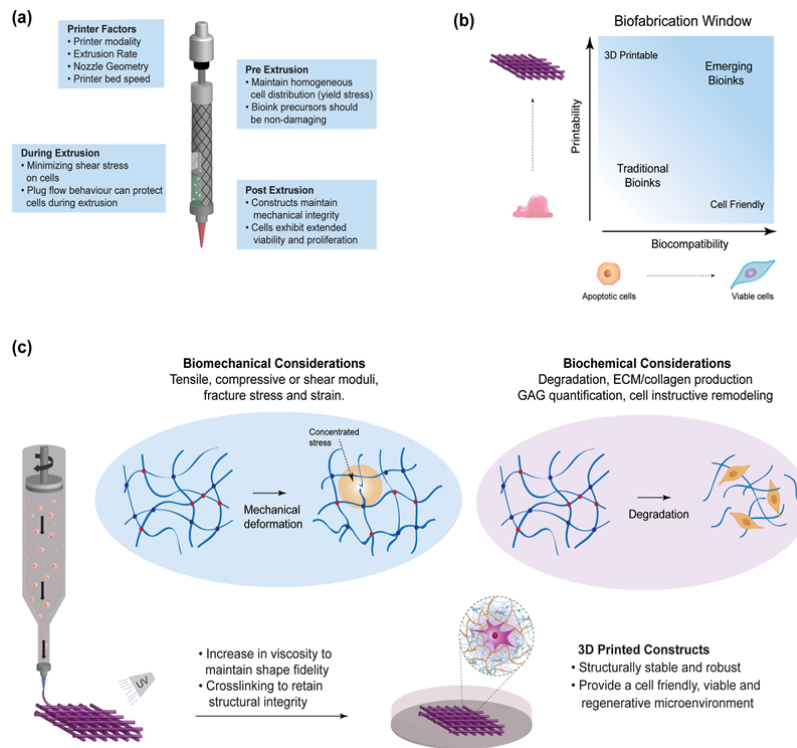
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		stains such as acridine orange, DNA with a micronucleus can be visualized. An increase in the frequency of micronuclei correlates to increased chromosomal damage.	
MTT/MTS/WTS	Cytoplasm/ Mitochondria	Tetrazolium dye is reduced to insoluble purple colored formazan by oxidoreductase in living cells. Assuming the similar cell types and cell numbers, the dyes can be used as a colorimetric assay for determining cell metabolic activity.	(237, 238)
JC-1 assay	Mitochondria	Aggregation of the dye is dependent on mitochondrial membrane potential. Upon aggregation, a shift in fluorescence occurs. This change in fluorescence can be used to determine mitochondrial membrane integrity.	(239- 241)



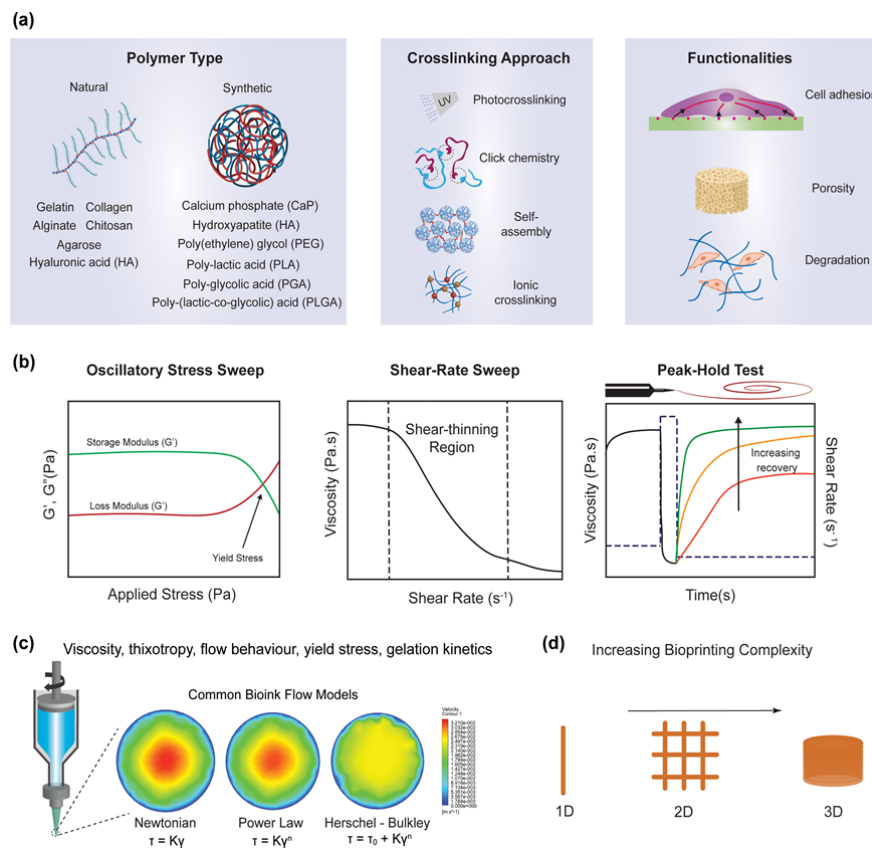
**Figure 1.** Trends in 3D Bioprinting. a) Exponential research growth in the field of 3D bioprinting. Data obtained from ISI Web of Science using “3D bioprinting”. (b) Publications in the field of 3D bioprinting focusing on various tissue types. Data obtained from ISI Web of Science, specifically looking at “3D bioprinting” and “bone/cartilage/vascular /skin/cardiac/liver/neural/skeletal/tendon or pancreas” (September 2019). c) Various applications of 3D bioprinting are explored in the field of pharmaceuticals, regenerative medicine and biomedical devices.



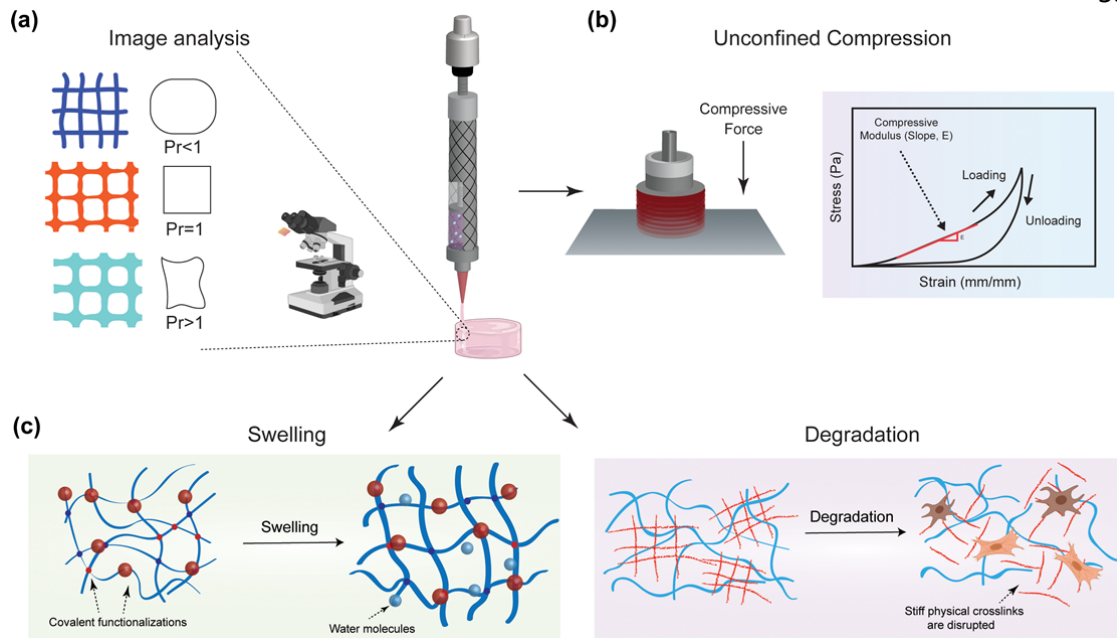
**Figure 2.** Considerations for extrusion-based 3D bioprinting. (a) Optimizing various printer modalities and pre, mid and post extrusion factors for ensuring favorable properties of the 3D bioprinted constructs. (b) Biofabrication window illustrating the trade-off between printability and biocompatibility required to make acceptable bioinks. (c) Biomechanical and biochemical considerations of the 3D bioprinted architectures. Coordinating cell-material interactions, mechanical properties of the materials and maintaining cellular viability governs 3D bioprinting proficiency.

This paper has been peer-reviewed and accepted for publication, but has yet to undergo copyediting and proof correction. The final published version may differ from this proof.

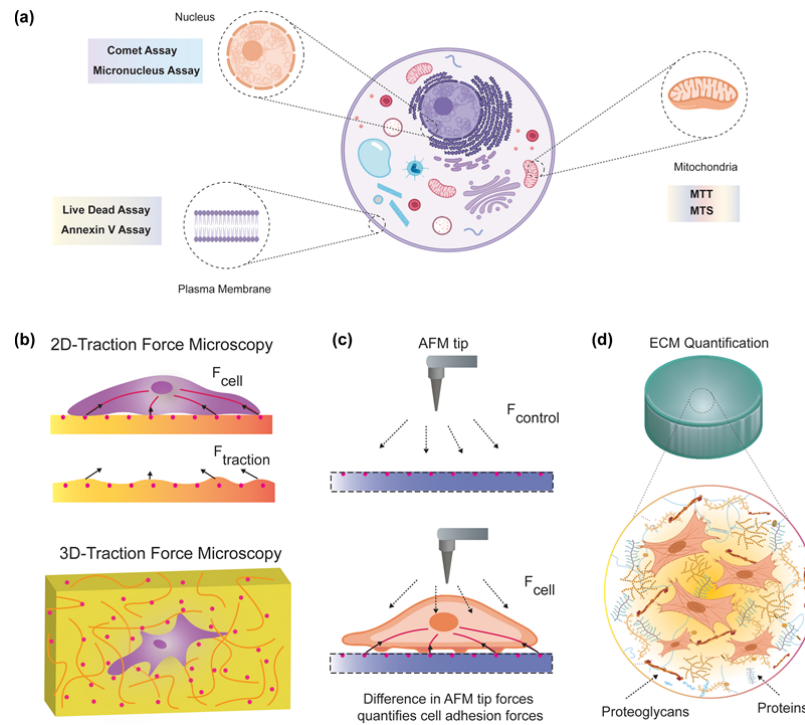




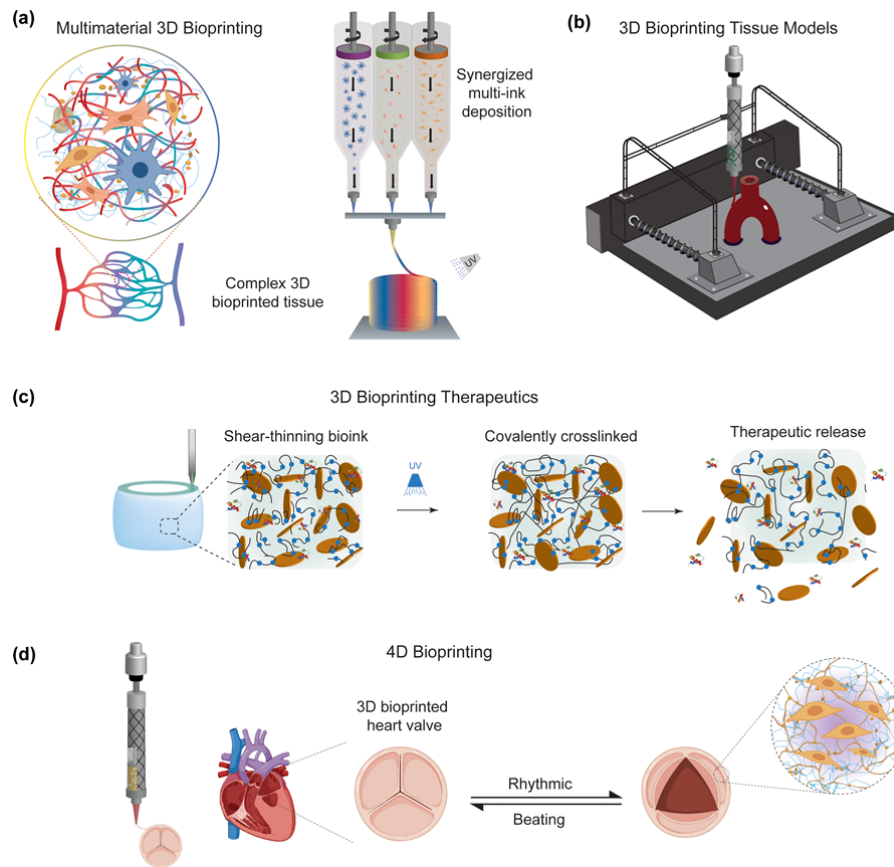
**Figure 3.** Pre-printing considerations. (a) Polymer selection is crucial in designing bioink with tunable performance. Type of polymer, crosslinking mechanisms and desired functionalities are important parameters which can be controlled to achieve enhanced cellular viability and material properties. (b) Rheological characterization is important to predict the utility of a bioink for 3D bioprinting. Oscillatory stress-sweep, peak-hold test, and shear-rate sweep experiments are important to determine printability of bioink. (c) The modelling of flow behavior provides distribution of stress within the bioink during the printing process. (d) Increasing bioprinting complexity also requires maintaining high shape fidelity for superior bioprinting and cellular proliferation in the constructs.



**Figure 4.** Post-printing considerations. (a) Optical image analysis is performed to examine the quality, spreading and printability of the bioinks post crosslinking. (b) Compressive mechanical analysis is performed to evaluate the mechanical stability and compressive modulus of the 3D bioprinted construct. (c) Swelling and degradation analysis aids in determining swelling ratio and degradation characteristics of the bioink, which is crucial in designing 3D bioprinted elements for specific tissue engineering applications.



**Figure 5.** Analyzing cell-material interactions. (a) Summary of various cellular cytotoxicity assays to monitor cellular viability post 3D bioprinting. (b) Traction force microscopy (TFM) analysis is used to determine the traction force cells generate when attached to the bioink. (c) Atomic force microscopy (AFM) techniques also quantify cell adherence to bioink through AFM cantilever deflections. (d) Extracellular matrix (ECM) quantification through various colorimetric assays determine how cells operate once encapsulated in the bioink, which is crucial as the 3D bioprinted scaffold simulates the native tissue 3D architecture.



**Figure 6.** Future Directions. (a) Multimaterial 3D bioprinting aims to recapitulate intricate composition of native tissue structures through printing multiple bioinks in a synergistic manner. (b) 3D bioprinting engineered tissue models enables conceiving *in-vitro* biomimetic tissue models which can be utilized in understanding disease progression and treatments for conditions such as cancer. (c) 3D bioprinting therapeutics utilizes bioinks engineered with protein therapeutics which can direct cell function in the bioprinted construct. (d) 4D bioprinting supports designing programmable structures with tunable behavior and functionalities. A bioprinted heart valve tissue is responsive to electrical impulses generated by cardiac cells and exhibits rhythmic contraction and expansion.

## Table of Contents

Extrusion-based 3D bioprinting is an emerging additive manufacturing approach for fabricating cell-laden tissue engineered constructs. The bioink properties control printability, fidelity and cellular viability. This review elucidates bioink considerations for pre- and post- printing processes and highlights new research directions in the field of bioink development and bioprinting.

**Keyword** 3D bioprinting, bioink, hydrogels, shear-thinning, additive manufacturing

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**Bioprinting 101: Design, Fabrication and Evaluation of Cell-laden 3D Bioprinted Scaffolds**

